

## **CHAPTER 2: MATHEMATICAL MODELLING**

### **A) Introduction**

- **The first step in analysis and design of a control system is to get the system specification**
- **Next is to get the block diagrams to represent the system operation**
- **Then, the schematic diagrams of subsystems are obtained, where the appropriate assumptions are made at this stage**
- **The following step is to get the mathematical modeling of the control system. For the electrical network modeling – Ohm’s Laws, Kirchoff’s Laws, etc. For mechanical system – Newton’s Laws, etc.**
- **Every subsystem in the overall system can be modeled separately and then combined together to get the overall system model.**
- **For the mathematical modeling, we have to know several basic mathematical concepts.**
- **A system represented by a differential equation is difficult to model as a block diagram. Hence, Laplace Transform is used to get the system’s transfer function with all initial conditions are assumed to be zero.**
- **The knowledge of how to use the Laplace Transform table (esp. the theorems) is very useful in modeling a system.**

Item no.	Theorem	Name
1.	$\mathcal{L}[f(t)] = F(s) = \int_{0^-}^{\infty} f(t)e^{-st} dt$	Definition
2.	$\mathcal{L}[kf(t)] = kF(s)$	Linearity theorem
3.	$\mathcal{L}[f_1(t) + f_2(t)] = F_1(s) + F_2(s)$	Linearity theorem
4.	$\mathcal{L}[e^{-at}f(t)] = F(s + a)$	Frequency shift theorem
5.	$\mathcal{L}[f(t - T)] = e^{-sT}F(s)$	Time shift theorem
6.	$\mathcal{L}[f(at)] = \frac{1}{a}F\left(\frac{s}{a}\right)$	Scaling theorem
7.	$\mathcal{L}\left[\frac{df}{dt}\right] = sF(s) - f(0^-)$	Differentiation theorem
8.	$\mathcal{L}\left[\frac{d^2f}{dt^2}\right] = s^2F(s) - sf(0^-) - \dot{f}(0^-)$	Differentiation theorem
9.	$\mathcal{L}\left[\frac{d^nf}{dt^n}\right] = s^nF(s) - \sum_{k=1}^n s^{n-k}f^{k-1}(0^-)$	Differentiation theorem
10.	$\mathcal{L}\left[\int_{0^-}^t f(\tau) d\tau\right] = \frac{F(s)}{s}$	Integration theorem
11.	$f(\infty) = \lim_{s \rightarrow 0} sF(s)$	Final value theorem <sup>1</sup>
12.	$f(0^+) = \lim_{s \rightarrow \infty} sF(s)$	Initial value theorem <sup>2</sup>

<sup>1</sup> For this theorem to yield correct finite results, all roots of the denominator of  $F(s)$  must have negative real parts and no more than one can be at the origin.

<sup>2</sup> For this theorem to be valid,  $f(t)$  must be continuous or have a step discontinuity at  $t = 0$  (i.e., no impulses or their derivatives at  $t = 0$ ).



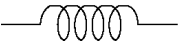
- **The concept of the transfer function has been looked into in the previous chapter. It can be obtained by transforming the differential equation into Laplace domain. (assuming zero initial conditions)**
- **For example, find the transfer function  $G(s) = C(s)/R(s)$  for the differential equation**

$$\frac{d^3c}{dt^3} + 3\frac{d^2c}{dt^2} + 7\frac{dc}{dt} + 5c = \frac{d^2r}{dt^2} + 4\frac{dr}{dt} + 3r$$

$$\rightarrow G(s) = \frac{C(s)}{R(s)} = \frac{s^2 + 4s + 3}{s^3 + 3s^2 + 7s + 5}$$

## B) Modelling of electrical systems

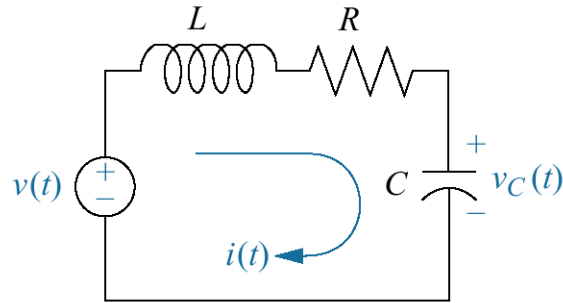
- Equivalent circuit for electrical networks consists of three passive linear components, which are resistors, capacitors and inductors
- The following table gives the components' relationships between voltage and current, and between voltage and charge under zero initial conditions:

 Capacitor	$v(t) = \frac{1}{C} \int_0^t i(\tau) d\tau$	$i(t) = C \frac{dv(t)}{dt}$	$v(t) = \frac{1}{C} q(t)$	$\frac{1}{Cs}$	$Cs$
 Resistor	$v(t) = Ri(t)$	$i(t) = \frac{1}{R} v(t)$	$v(t) = R \frac{dq(t)}{dt}$	$R$	$\frac{1}{R} = G$
 Inductor	$v(t) = L \frac{di(t)}{dt}$	$i(t) = \frac{1}{L} \int_0^t v(\tau) d\tau$	$v(t) = L \frac{d^2 q(t)}{dt^2}$	$Ls$	$\frac{1}{Ls}$

Note: The following set of symbols and units is used throughout this book:  $v(t) = \text{V}$  (volts),  $i(t) = \text{A}$  (amps),  $q(t) = \text{Q}$  (coulombs),  $C = \text{F}$  (farads),  $R = \Omega$  (ohms),  $G = \text{M}$  (mhos),  $L = \text{H}$  (henries).

- We can combine those electrical components into circuits, decide the input and output, and then find the transfer function.
- We can sum voltage around loops or sum currents at nodes, depending on which technique involves less effort.
- From these relations, we can write the differential equations for the circuit, take the Laplace transforms of the differential equations and finally solve for the transfer function.

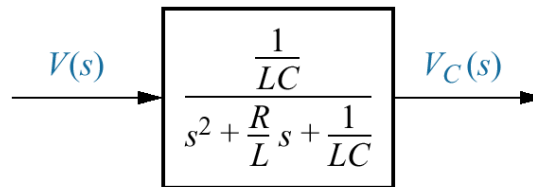
- **Example: Find the transfer function relating the capacitor voltage,  $V_c(s)$  to the input voltage,  $V(s)$ .**



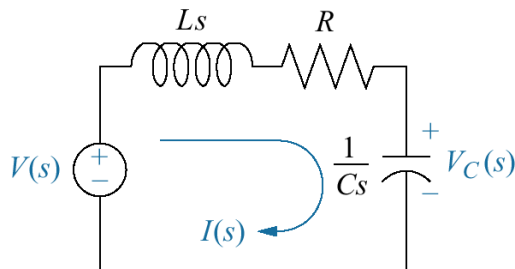
$$L \frac{di(t)}{dt} + Ri(t) + \frac{1}{C} \int_0^t i(t) dt = v(t)$$

$$LC \frac{d^2 v_c(t)}{dt^2} + RC \frac{dv_c(t)}{dt} + v_c(t) = v(t)$$

$$(LCs^2 + RCs + 1)V_c(s) = V(s)$$

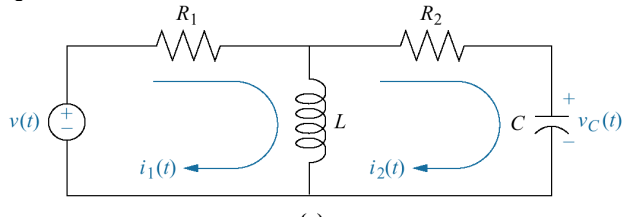


- **The problem can also be simplified by transforming the circuit into the Laplace s-domain.**

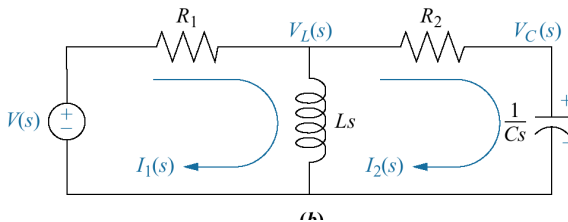


**Using the voltage division technique to get the required transfer function.**

- For multiple loop network:



Transform the circuit into s-domain:



Depending on the number of loops in the circuit, obtain the simultaneous equations according to this rule:

$$[\Sigma \text{ imp Mesh1}]I_1(s) - [\Sigma \text{ common imp}]I_2(s) = [\Sigma \text{ voltage applied Mesh1}]$$

$$- [\Sigma \text{ common imp}]I_1(s) + [\Sigma \text{ imp Mesh2}]I_2(s) = [\Sigma \text{ voltage applied Mesh2}]$$

ie,

$$\begin{bmatrix} R_1 + Ls & -Ls \\ -Ls & Ls + R_2 + \frac{1}{Cs} \end{bmatrix} \begin{bmatrix} I_1(s) \\ I_2(s) \end{bmatrix} = \begin{bmatrix} V(s) \\ 0 \end{bmatrix}$$

**Cramer's rule (or any other method) can be used to solve the simultaneous equations as required:**

$$I_2(s) = \frac{\begin{vmatrix} R_1 + Ls & V(s) \\ -Ls & 0 \end{vmatrix}}{\begin{vmatrix} R_1 + Ls & -Ls \\ -Ls & Ls + R_2 + \frac{1}{Cs} \end{vmatrix}}$$

**to give**

$$V(s) \rightarrow \boxed{\frac{LCs^2}{(R_1 + R_2)LCs^2 + (R_1R_2C + L)s + R_1}} I_2(s)$$

**- For three-loop network,**

